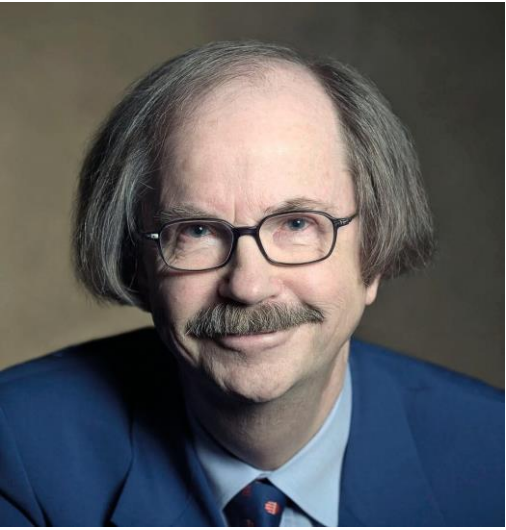


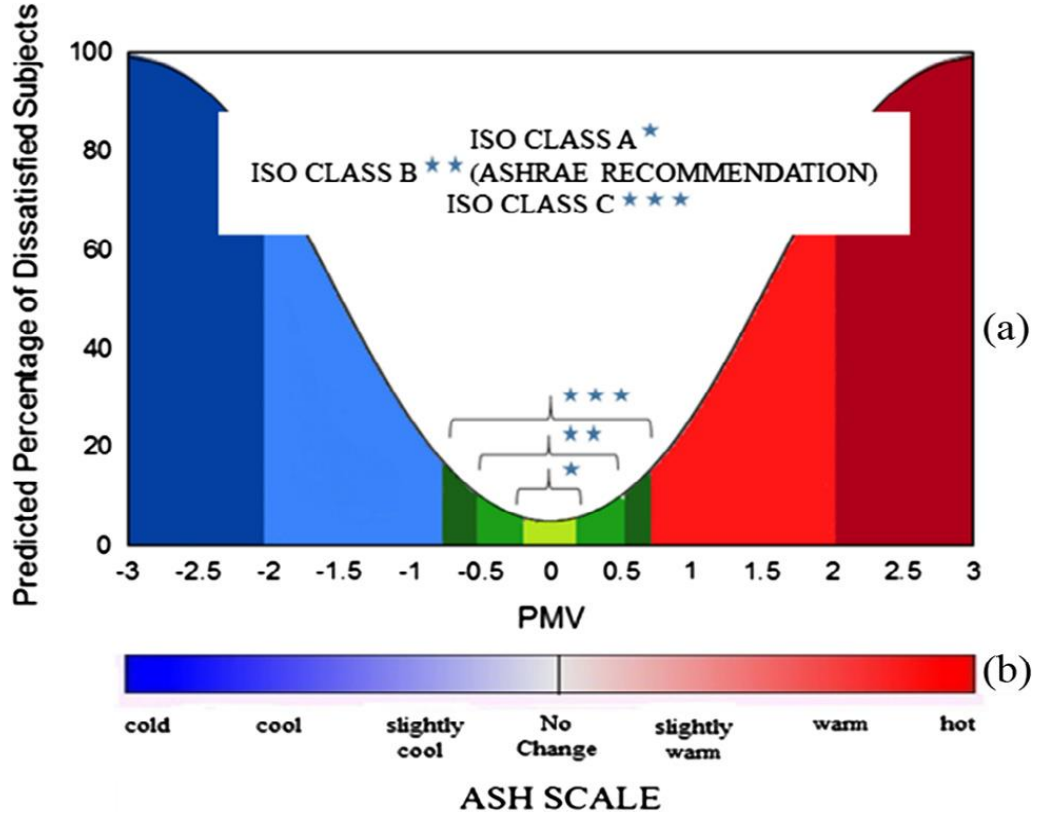
New thermal comfort indices based on iso-comfort arrays

Sulin A.B., Ryabova T.V., Sankina I.N., Nikitin A.A., Muraveinikov S.S.

Thermal Comfort Indices by P.O. Fanger



P.O. Fanger

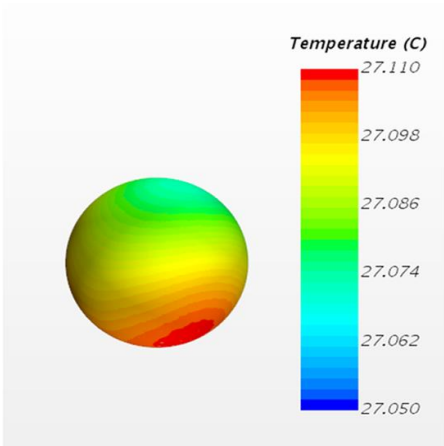
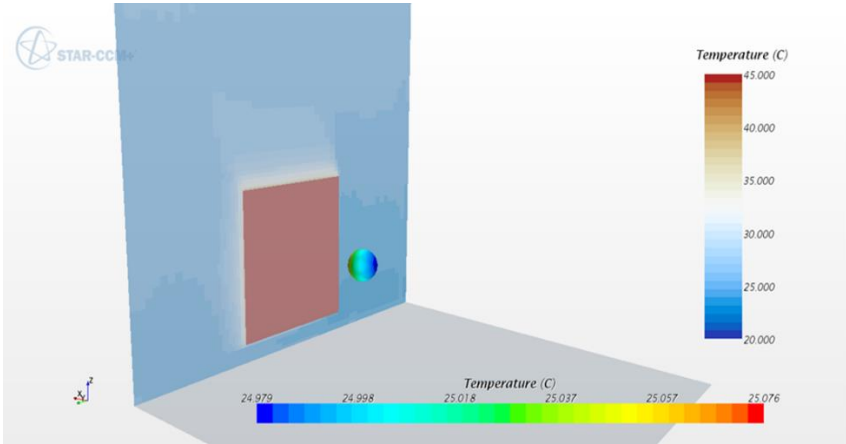


PMV – PPD relation

Radiative factor of thermal comfort



Globe thermometer



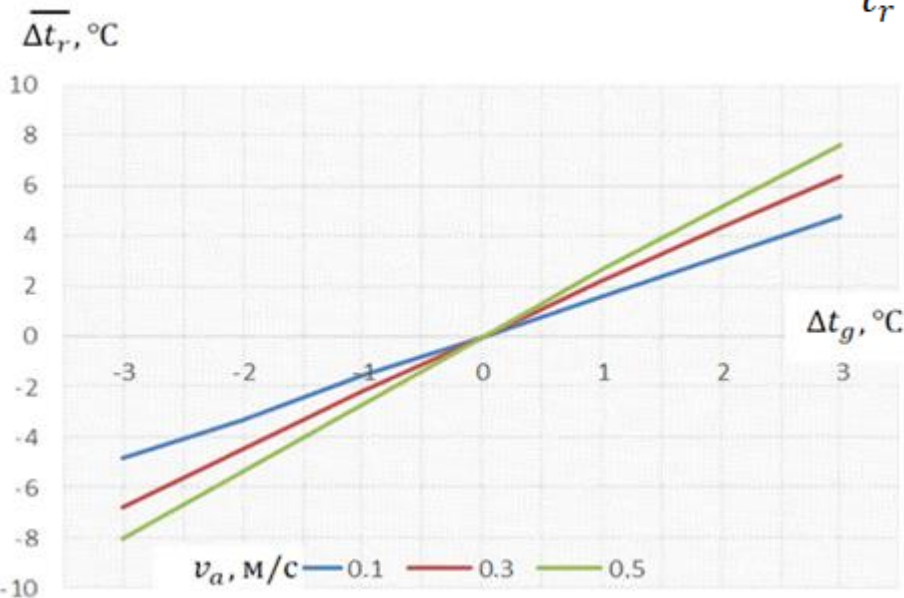
CFD modeling

Mean radiative temperature

New factors:

- *mean radiative temperature difference*
- *globe thermometer temperature difference*

$$\bar{t}_r = \left[(t_g + 273)^4 + \frac{1,1 \cdot 10^8 \cdot v_a^{0,6}}{\varepsilon D^{0,4}} \cdot (t_g - t_a) \right]^{\frac{1}{4}} - 273.$$



Mean radiative temperature difference
vs
globe thermometer`s temperature difference

$$\Delta t_r = t_r - t_a$$

$$\Delta t_g = t_g - t_a$$

Formation of iso-comfort arrays

PMV = +0.49

$\Delta t_p, ^\circ\text{C}$

v = 0.1, m/s

v = 0.3, m/s

v = 0.5, m/s

v = 0.7, m/s

-8

27.60

27.63

29.27

27.65

-4

25.81

26.29

28.10

26.63

0

23.98

24.92

26.90

25.59

4

22.12

23.52

25.67

24.51

8

20.356

22.08

22.901

23.41

PMV = -0.49

$\Delta t_p, ^\circ\text{C}$

v = 0.1, m/s

v = 0.3, m/s

v = 0.5, m/s

v = 0.7, m/s

-8

23.23

23.72

23.94

24.066

-4

21.45

22.40

22.81

23.06

0

19.63

21.04

21.65

22.03

4

17.80

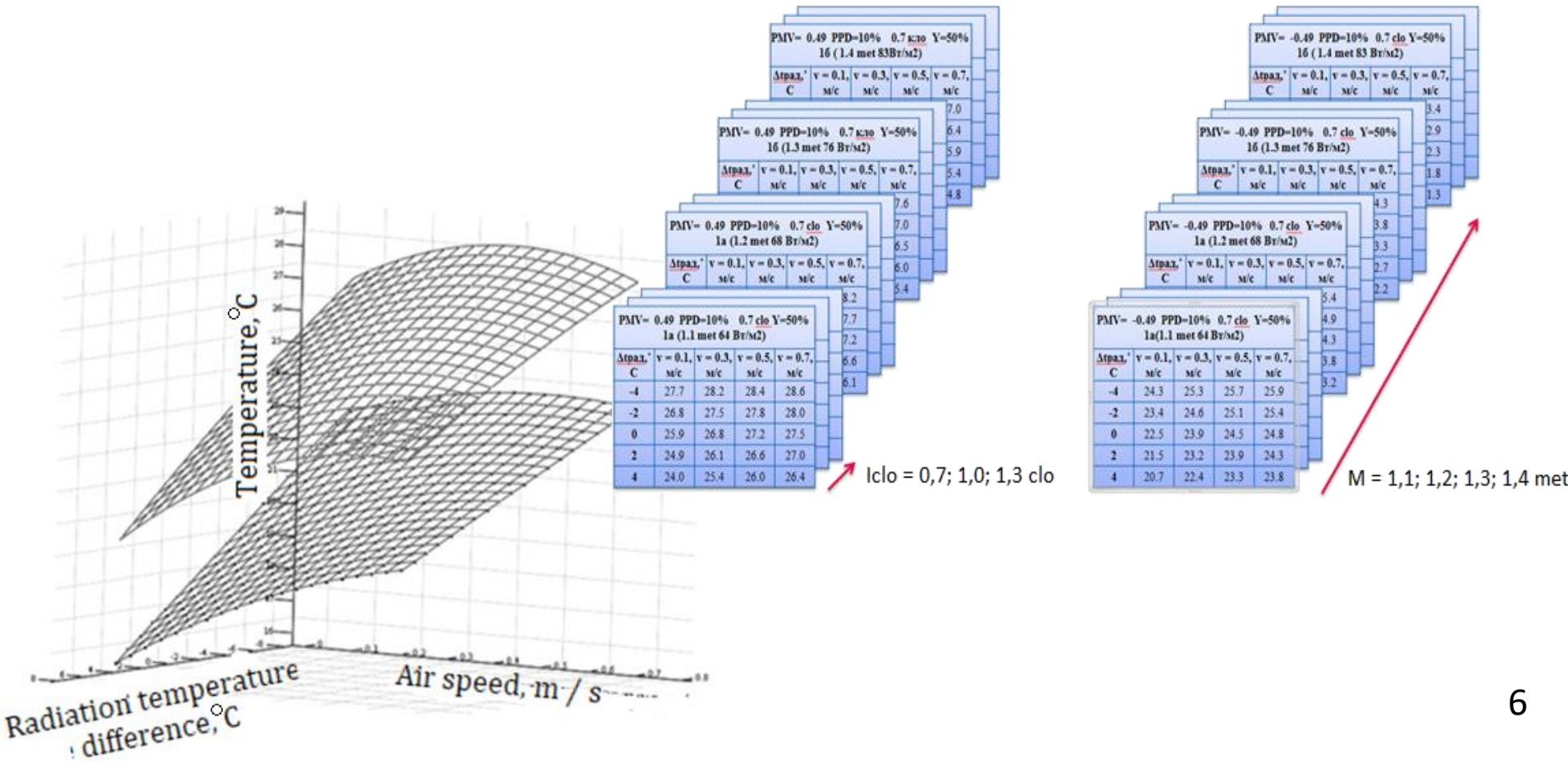
19.65

20.46

20.07

Comfort class: B
Activity: 1.1 met
Clothes: 1.0 clo

Iso-comfort arrays data base



Equivalent comfort temperature

Equivalent temperature by Madsen T. L. (ASHRAE trans. - 1984. - T. 90):

$$t_{eq} = 0.55 * t_a + 0.45 * \bar{t}_r + \frac{0.24 - 0.75\sqrt{v_a}}{1 + I_{cl}} (36.5 - t_a)$$

New index: equivalent comfort temperature:

$$t_{eqc} = 0.55 * t_{ac} + 0.45 * \bar{t}_{rc} + \frac{0.24 - 0.75\sqrt{v_{ac}}}{1 + I_{cl}} (36.5 - t_{ac})$$

Equivalent comfort temperature data base

Comfort class: B Activity: 1.1 met Clothes: 1.0 clo
 Calculation example

PMV = +0.49				
$\Delta t_p, ^\circ\text{C}$	v = 0.1, m/s	v = 0.3, m/s	v = 0.5, m/s	v = 0.7, m/s
-8	24.5	24.1	23.7	23.4
-4	24.5	24.2	23.9	23.7
0	24.4	24.4	24.2	23.9
4	24.4	24.5	24.5	24.2
8	24.4	24.6	24.6	24.4
	Mean value 24.2		Deviation 0.3	
PMV = -0.49				
$\Delta t_p, ^\circ\text{C}$	v = 0.1, m/s	v = 0.3, m/s	v = 0.5, m/s	v = 0.7, m/s
-8	20.4	20.1	19.8	19.4
-4	20.4	20.3	20.0	19.7
0	20.4	20.5	20.2	20.0
4	20.4	20.6	20.5	20.2
8	20.4	20.7	20.7	20.5

PMV = + 0.49			
	0.7 clo	1.0 clo	1.3 clo
1.1 met	25.7	24.2	22.8
1.2 met	25.3	23.8	22.3
1.3 met	24.5	22.9	21.3
1.4 met	23.8	22.1	20.4
PMV = - 0.49			
	0.7 clo	1.0 clo	1.3 clo
1.1 met	22.7	20.3	18.2
1.2 met	21.8	19.5	17.3
1.3 met	20.5	18.0	15.6
1.4 met	19.4	16.8	14.2

Comfort class: B
 Summarized data

Equivalent comfort temperature calculation (RU Patent No 2682872)

Comfort class ISO 7730	Thermal sensation PMV	Equivalent comfort temperature
A	+0.19	$t_{eqc} = 47.69 * 0.67^{met} * 0.76^{clo}$
	-0.19	$t_{eqc} = 56.10 * 0.58^{met} * 0.70^{clo}$
B	+0.49	$t_{eqc} = 43.23 * 0.73^{met} * 0.80^{clo}$
	-0.49	$t_{eqc} = 66.49 * 0.51^{met} * 0.65^{clo}$
C	+0.69	$t_{eqc} = 40.69 * 0.77^{met} * 0.82^{clo}$
	-0.69	$t_{eqc} = 72.58 * 0.47^{met} * 0.62^{clo}$

Operative (*resulting, effective*) comfort temperature

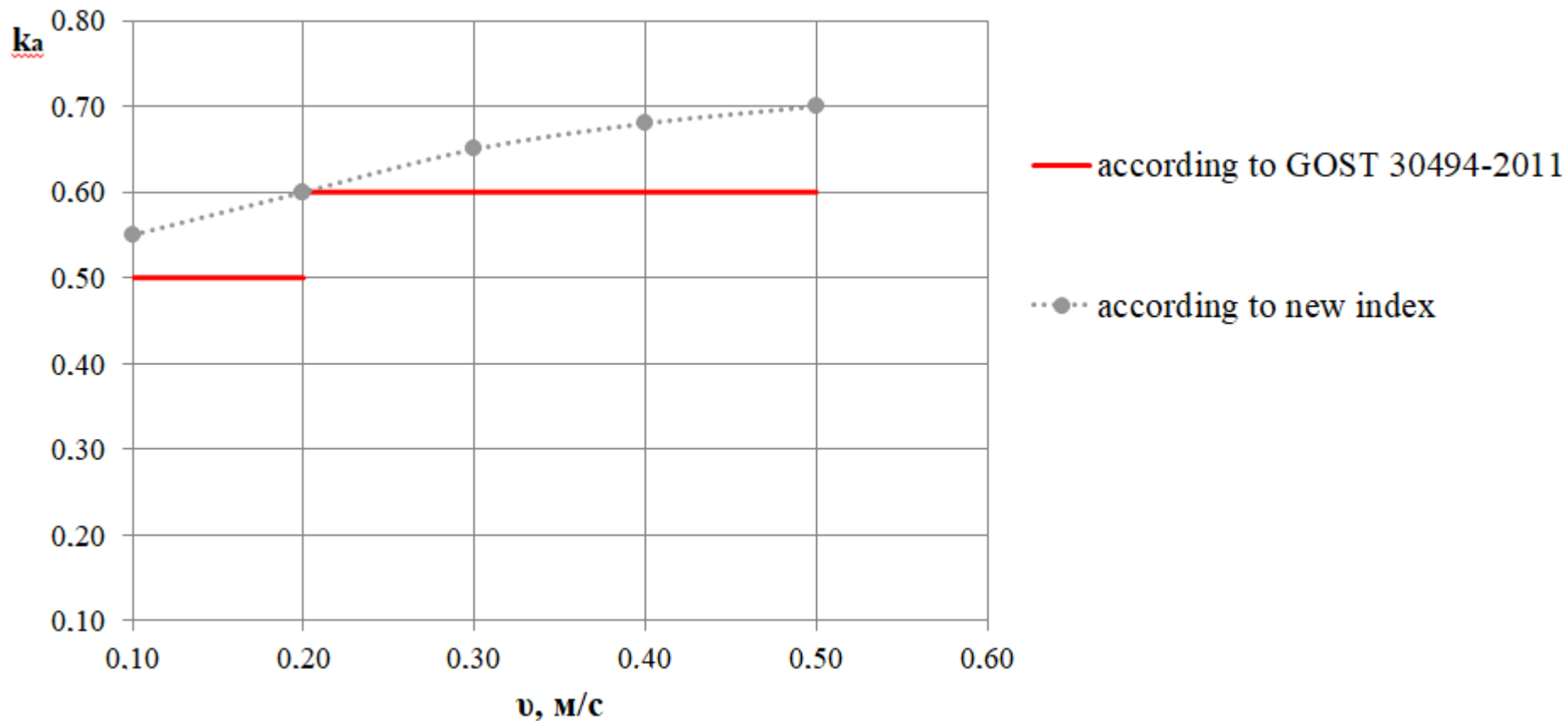
	0.1	0.2	0.3	0.4	0.5	
-6	18.47	18.95	19.29	19.46	19.65	Iso-comfort array
-4	17.60	18.25	18.61	18.88	19.07	
-2	16.69	17.51	17.98	18.30	18.54	
0	15.78	16.74	17.30	17.66	17.94	
2	14.95	16.01	16.65	17.07	17.41	
4	14.11	15.25	15.98	16.46	16.82	
6	13.34	14.50	15.26	15.81	16.21	
	0.1	0.2	0.3	0.4	0.5	Operative comfort temperature
-6	15.77	16.61	17.19	17.54	17.85	
-4	15.8	16.69	17.21	17.60	17.87	
-2	15.79	16.73	17.28	17.66	17.94	
0	15.78	16.74	17.30	17.66	17.94	
2	15.85	16.79	17.35	17.71	18.01	
4	15.91	16.81	17.38	17.74	18.02	
6	16.04	16.84	17.36	17.73	18.01	
Mean value	15.84857	16.74429	17.29571	17.66286	17.94857	
Deviation	0.097541	0.078285	0.07413	0.072736	0.069144	
Weight ratio for t_a	0.55	0.61	0.65	0.68	0.7	
Weight ratio for t_r	0.45	0.39	0.35	0.32	0.3	

New index

$$t_o^* = k_a \cdot t_a + (1 - k_a) \cdot t_r$$

$$k_a = -0.64 \cdot v^2 + 0.76 \cdot v + 0.48$$

New operative temperature wight ratio



Operative temperature: 3 calculate methods

ANSI/ASHRAE Standard 55

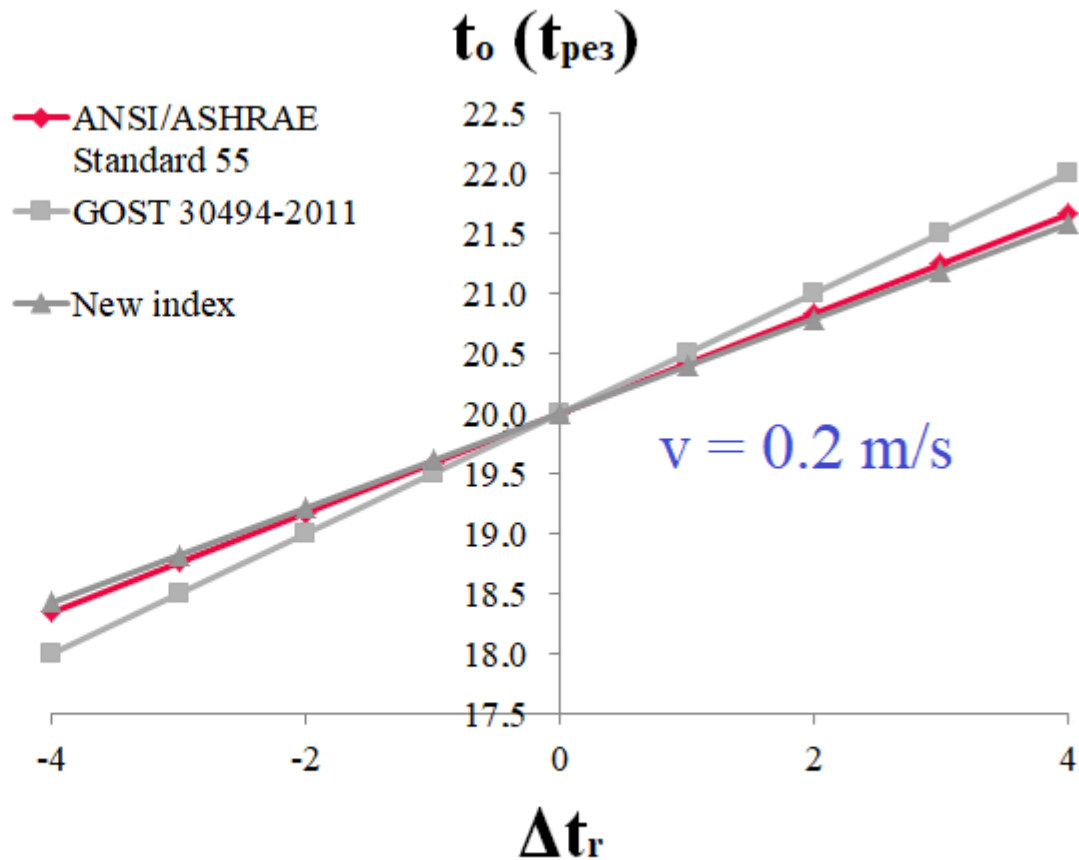
$$t_o = \frac{t_r + t_a \cdot \sqrt{10v}}{1 + \sqrt{10v}}$$

GOST 30494-2011

$$t_o = \frac{t_a + t_r}{2} \text{ for } v \leq 0.2$$
$$t_o = 0.6t_a + 0.4t_r$$

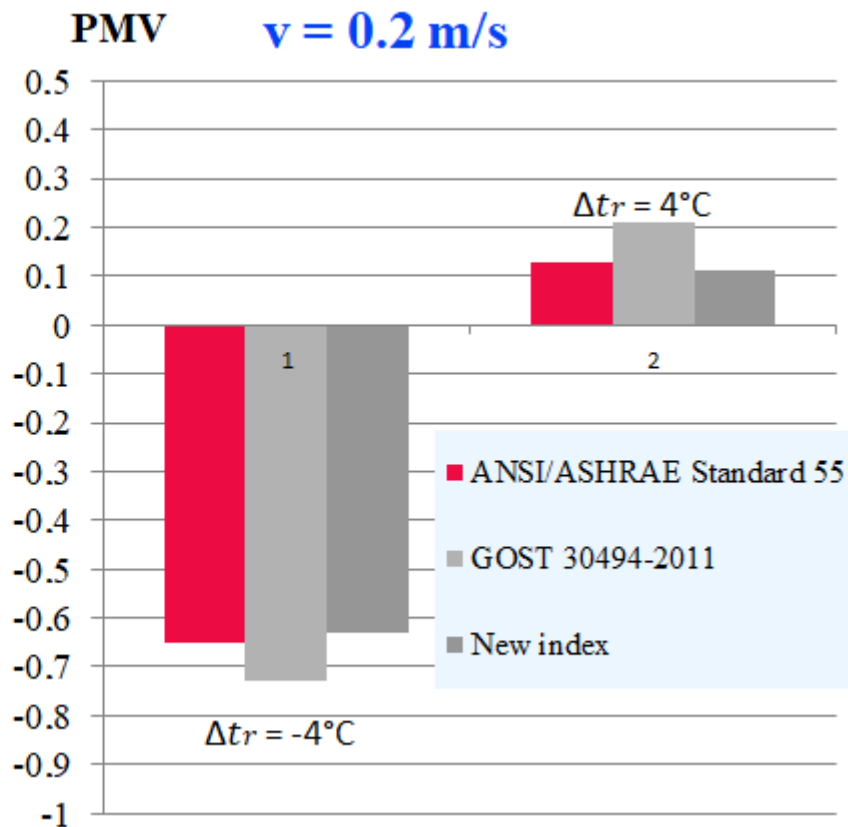
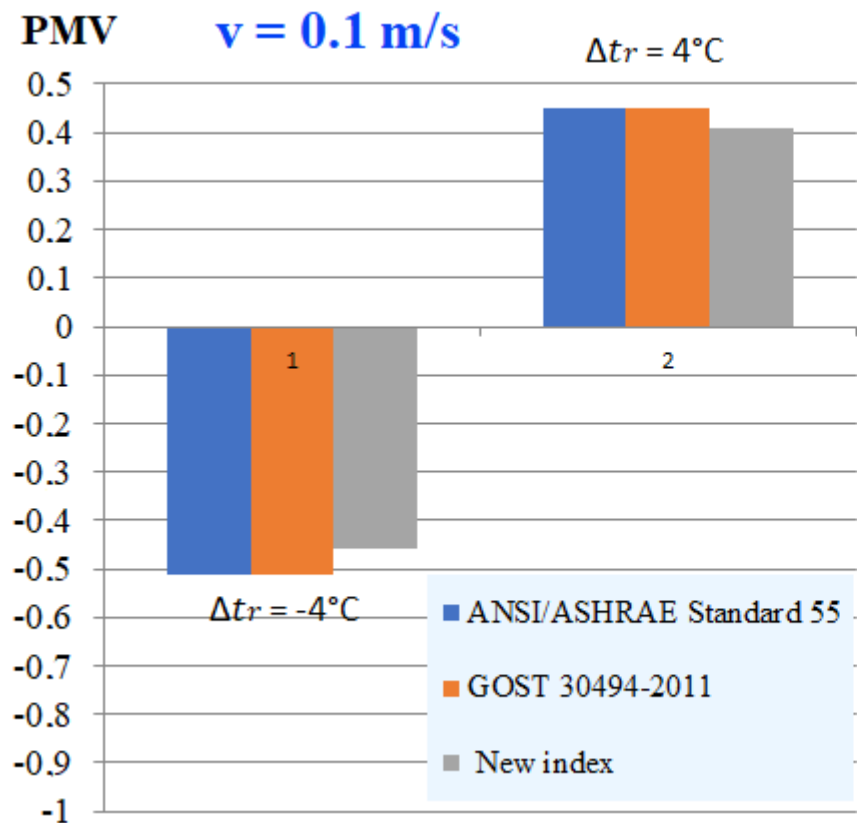
New index

$$t_o^* = (-0.64v^2 + 0.76v + 0.48) \cdot t_a + (0.64v^2 - 0.76v + 0.52) \cdot t_r$$



Predicted mean vote of thermal comfort

based on operative comfort temperature ($t_a = +23^\circ\text{C}$)



Conclusions

1. New concepts have been introduced:
 - isocomfortable parameters matrix;
 - equivalent comfort temperature;
 - radiation temperature difference;
 - the temperature difference of the ball thermometer;
 - operational (resulting) comfortable temperature.
2. Generalized calculated expressions for the premises microclimate parameters of three comfort classes according to ISO 7730 have been obtained and patented.
3. New weighting factors were obtained for determining the operating temperature based on the method of P.O. Fanger.
4. It is shown that the use of a new method for calculating the operating temperature leads to an increase in the expected thermal comfort level in the room.

Thank you for attention

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